

Appl. No. 10/807,524
Amtd. dated Aug. 18, 2005
Reply to Office Action of May 18, 2005

Amendments to the Specification:

Please replace paragraph 0005 (page 1, lines 9-20) with the following amended paragraph:

[0005] The Cellular Telecommunications and Internet Association (CTIA) operates an equipment testing and certification program to ensure high-quality and reliability of cellular, personal communication services (PCS), enhanced specialized mobile radio (ESMR), and mobile satellite services products. Within ~~Included within~~ this program, the CTIA establishes requirements for spherical-scanning antenna measurement systems (i.e., anechoic chambers). One challenge to antenna testing system designers is meeting the CTIA requirements while maintaining moderate range distances and ceiling heights. To meet the CTIA's antenna measurement system requirements [[do so]] efficiently, a measurement antenna that is low profile, dual-polarized, and multi-band is desired. The antenna preferably has a directive radiation pattern with high symmetry and low taper across the main beam, as well as low cross-polarization levels. It is also desirable that a single antenna assembly be capable of measuring in multiple bands and modes[[,]] to increase throughput.

Please replace paragraph 0007 (page 2, lines 7-9) with the following amended paragraph:

[0007] For spherical-scanning ranges, the length of the a probe antenna having a high profile in the direction of radiation will reduce the range distance and consequently degrade measurement certainty, uncertainty, and thus, an antenna with a very low profile is desirable.

Please replace paragraph 0008 (page 2, lines 10-18) with the following amended paragraph:

[0008] A stacked patch antenna is a good candidate for this application. Single-ended-fed ("single-fed") Single-ended-feed stacked patch antennas patches are well-known in antenna literature as an approach for broad band or multi-band operation. However, to obtain ~~For the~~ required bandwidths typically required for a spherical-scanning test system [[this]] application, however, the patch antenna height is required to be large relative to the heights of single-fed patch antennas [[that]] of the known art. At such ~~For this~~ element height, a single-fed

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implementation suffers pattern asymmetry and increased cross-polarization. The high-frequency element of the antenna pattern is also more susceptible to diffraction/reflection effects from the low-frequency ground plane, which may cause ripple in the pattern peak. Such pattern ripple [[This]] increases the difficulty in satisfying required to satisfy the CTIA requirements.

Please replace paragraph 0010 (page 2, lines 20-24) with the following amended paragraph:

[0010] The accompanying figures, where like reference numerals refer to identical or functionally similar elements throughout the separate views and which together with the detailed description below[[,]] are incorporated in and form part of the specification, serve to further illustrate various embodiments and to explain various principles and advantages all in accordance with the present invention.

Please replace paragraph 0016 (page 3, lines 7-15) with the following amended paragraph:

[0016] As required, detailed embodiments of the present invention are disclosed herein; however, it is to be understood that the disclosed embodiments are merely exemplary of the invention, which can be embodied in various forms. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but rather should be interpreted merely as a basis for the claims and as a representative basis for teaching one skilled in the art to variously employ the present invention in virtually any appropriately detailed structure. Further, the terms and phrases used herein are not intended to be limiting; but rather[[,]] are intended to provide an understandable description of the invention.

Please replace paragraph 0017 (page 3, line 16 through page 4, line 3) with the following amended paragraph:

[0017] The terms "a" or "an," as used herein, are defined as one or more than one. The term "plurality," as used herein, is defined as two or more than two. The term "another," as used herein, is defined as at least a second or more. The terms "including" and/or "having," as used

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herein, are defined as comprising (i.e., open language). The term "coupled," as used herein, is defined as connected, although not necessarily directly, and not necessarily mechanically. The terms "program," "software application," and the like, as used herein, are defined as a sequence of instructions designed for execution on a computer system. A program, computer program, or software application may include a subroutine, a function, a procedure, an object method, an object implementation, an executable application, an applet, a servlet, a source code, an object code, a shared library/dynamic load library and/or other sequence of instructions designed for execution on a computer system.

Please replace paragraph 0018 (page 4, lines 4-17) with the following amended paragraph:

[0018] The present invention utilizes one or more patch antennas with a large height and air for the dielectric to get a large, single-mode bandwidth of operation in a light-weight structure. The one or more patch antennas are "fed" differentially at two symmetrical points to ensure that only one mode of radiation exists[[,]] for each of the two orthogonal linear polarizations supported by the patch antenna. In accordance with the present invention, the frequency of operation for each patch antenna is arbitrarily selected. A centrally located, fully grounded conduit is used which allows independent transmission lines to be run to the upper patches. In one embodiment of the present invention, all of the switching and control hardware is integrated onto a micro strip printed circuit board. Multi-band, dual-polarized probe antennas include significant circuitry to be able to connect each of the antenna capabilities to the output connectors on demand. By integrating the circuitry into the patch antenna structure, all of the antenna's capability may be available by using control signals from the transmission lines used to connect the probe antennas to the instrumentation.

Please replace paragraph 0019 (page 4, line 18 through page 5, line 2) with the following amended paragraph:

[0019] FIG. 1 is a cross sectional view of one embodiment of a differential-fed stacked patch antenna 100 in accordance with the present invention. The stacked patch antenna 100 preferably

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comprises two or more patch antennas that are superimposed. If X and Y axes define the plane in which the bottom-most patch antenna's ground plane lies, and the Z axis lies in the direction of displacement of the patch element from the ground plane, the successive patches are arrayed along the Z axis relative the bottom-most patch[[.]] (i.e., symmetrically aligned around the Z-axis). Preferably, the patch element of a lower patch antenna in the stack also serves as the ground plane element for the next higher patch antenna in the stack.

Please replace paragraph 0021 (page 5, line 13 through page 6, line 6) with the following amended paragraph:

[0021] FIG. 2 illustrates one embodiment of a patch antenna for use in accordance with the present invention. As an example, the patch antenna can be the first patch antenna 105 and/or the second patch antenna 110 of FIG. 1. Specifically, FIG. 2 is a top plan view of a single-polarization, differential feed patch antenna 200. As illustrated in FIG. 2, the single-polarization, differential feed patch antenna 200 comprises a grounded substrate 220; a radiating system 210 carried, supported by, or suspended over the grounded substrate 220, and a feed system 230 having two feed points 205, 215. The grounded substrate 220, for example, can be formed by a layer of dielectric material[[.]] and a layer of conductive material that functions as a ground plane. In one embodiment, the dielectric material used is an alumina substrate, which has a dielectric constant of approximately ten (10). Alternatively, the dielectric material may be air, as described above. The feed system 230 can include a micro strip line[[.]] disposed beneath the ground plane of the grounded substrate 220. Preferably, the feed points 205,215 of the feed system 230 are each comprised of a coaxial feed rod coupled to the micro strip line to provide a conduit for communication signals. The feed points 205, 215, in accordance with one embodiment of the present invention, are structurally located along the same axis (i.e., in a straight line) with relation to each other.

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Please replace paragraph 0022 (page 6, lines 7-15) with the following amended paragraph:

[0022] As is known in the art, the radiating system 210 can include a patch radiator that forms a resonating structure[[,]] when excited by a feed signal. The patch radiator is preferably rectangular in geometry, having a length measured in a direction of wave propagation (herein referred to as "resonating length")[[,]] and a width measured perpendicular to the resonating length. For dual-polarization implementations, a square patch element provides two orthogonal linear polarizations. Those of ordinary skill in the art will recognize that shapes other than a square (for example, a circle) can also be employed to support the desired modes of operation in accordance with the present invention.

Please replace paragraph 0023 (page 6, line 16 through page 7, line 2) with the following amended paragraph:

[0023] FIG. 3 illustrates an alternate embodiment of a patch antenna for use in accordance with the present invention. As an example, the patch antenna can be the first patch antenna 105 and/or the second patch antenna 110 of FIG. 1. Specifically, FIG. 3 is a top plan view of a dual-polarization, differential feed patch antenna 300. As illustrated in FIG. 3, the dual-polarization, differential feed patch antenna 300 comprises a grounded substrate 220,[[;]] a radiating system 210 carried or supported by the grounded substrate 220, and a feed system 330 comprised of two pairs 305, 310 of feed points (315, 335 and 325, 320 respectively). As illustrated, the two pairs 305, 310 of feed points feedpoints are preferably orthogonally located with respect to each other. Preferably, the feed points 315, 320, 325, 335 are each comprised of a coaxial feed rod coupled to the micro strip line to provide a conduit for communication signals.

Please replace paragraph 0024 (page 7, line 3 through page 8, line 15) with the following amended paragraph:

[0024] Referring back to FIG. 1, the stacked patch antenna 100 further comprises a plate 115 for mounting the entire assembly of the stacked patch antenna 100 and providing rigidity to the

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structure. A control circuit board 120 is mechanically located at a fixed distance from the plate 115 using one or more lower spacers 125. One or more ground planes 130 are electrically and mechanically coupled to the control circuit board 120. The ~~one or more~~ ground planes 130 serve as an earth ground or reference for the stacked patch antenna 100. One or more feed rods 135 couple the control circuit board 120 to a circuit board 175 located between the first patch antenna 105 and the second patch antenna 110. The circuit board 175 serves as both the radiating patch element for the second patch antenna 110 and the ground plane element of the first patch antenna 105. The control circuit board 120 preferably includes all of the switching and control hardware integrated onto a micro strip printed circuit board. Multi-band, dual-polarized probe antennas include significant circuitry to be able to connect each of the antenna capabilities to the output connectors on demand. By integrating the circuitry, all of the capability may be available by using control signals from the transmission lines used to connect the probe antennas (i.e., the stacked patch antenna 100) to the instrumentation. One or more coaxial cable feed lines 140 electrically couple the control circuit board 120 to the circuit board 175. These coaxial cables 140 carry the feed signal(s) to the first patch antenna 105. The circuit board 175 distributes the signal(s) from the ~~one or more~~ coaxial cable feed lines 140 to one or more [[the]] feed rods 170. The ~~one or more~~ feed rods 135 and the ~~one or more~~ coaxial cable feed lines 140 connect the second and first patch antennas 110 and 105, respectively, to the transceiver circuitry located within the control circuit board 120 to transfer radio-frequency (RF) energy between the two elements. Preferably, the ~~one or more~~ coaxial cable feed lines 140 are comprised of coaxial cable. To provide mechanical rigidity, a control circuit side bushing 145 and a patch antenna side bushing 150 are coupled to shield conductors on opposing ends of the ~~one or more~~ coaxial cable feed lines 140. One or more middle spacers 155 provide further mechanical support to locate the circuit board 175 at a fixed distance from the plate 115. One or more nylon studs 160 are located within the middle spacers 155 to mechanically support the circuit board 175. The patch element of the first patch antenna 105 is located at a fixed distance above the circuit board 175 using one or more top spacers 165. One or more nylon screws 180 connected to the spacers 165 through the first patch antenna 105 hold the entire assembly of the stacked patch antenna 100 together. Communication signals to the stacked patch antenna 100 are coupled through one or more SMA/SMB adapters 185 and one or more blind mate adapters 190.

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Please replace paragraph 0026 (page 8, line 22 through page 9, line 9) with the following amended paragraph:

[0026] As is known by those of ordinary skill in the art, a differential feed arrangement is one in which a structure is excited by two signals which have the same amplitude, but a (nominal) 180-degree difference in phase. This contrasts with a single-ended feed, in which a structure is excited by only a single signal referenced to ground. A common means of implementing a differential feed is to split the excitation RF (radio frequency) signal (for example, with a 3-dB splitter) and then to apply an additional 180-degree phase shift to only one of the splitter outputs. This yields two RF signals, referenced to ground, with identical amplitudes, but a relative phase shift of 180 degrees. Such a signal-splitting, phase-shifting approach [[(This)] is sometimes implemented as a single circuit operation[[,]] using a 180-degree hybrid.[D]] The [[These]] two signals are then applied to two appropriate feed points feedpoints on the structure, as defined for the desired structural mode to be excited.

Please replace paragraph 0027 (page 9, lines 10-18) with the following amended paragraph:

[0027] In accordance with the present invention, for each polarization, these two feed points feedpoints lie on a centerline of the patch element[[,]] and are symmetrically located on that centerline about the patch element's centroid (i.e., a center point). The distance of the feed points feedpoints from the centroid is adjusted so as to achieve the desired impedance match at the frequency of operation. Since the present invention often is desired to provide two orthogonal polarizations from one structure, a second polarization is excited on the square patch structure, using an identical differential pair of feeds[[,]] rotated geometrically 90 degrees about the patch centroid relative to the first polarization's feeds, so as to lie on the patch's other centerline.

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Please replace paragraph 0028 (page 9, line 19 through page 10, line 10) with the following amended paragraph:

[0028] Each of the first patch antenna 105 and the second patch antenna 110 are "fed" differentially at two symmetrical points to ensure that only one mode of radiation exists[[.]] for each of the two orthogonal linear polarizations supported by the patch antenna[[. .]] (e.g., as illustrated in FIG. 2 previously herein). In a preferred embodiment, the first patch antenna 105 is differentially fed using four feeds (400, 405, 410, and 415) as two pairs (400, 410 and 405, 415), such [[()]] as illustrated in FIG. 3 previously herein[[()]]. Each pair (400, 410 and 405, 415) provides separate linear excitations. The second patch antenna 110 is similarly differentially fed using four feed rods 135, similarly arranged as pairs, not visible in FIG. 4. The pairs, as illustrated, preferably are located as pairs on a clock face (e.g., at 12 and 6,[[D]] and [[()]] at 3 and 9). The present invention further utilizes a centrally located, fully grounded conduit, comprising the shield conductors of the coaxial cables 140, that allows independent transmission lines to be run to the upper patches (e.g., [[i.e.]] first patch antenna 105). Because this grounded conduit passes through the center of the second patch antenna 110, which is a zero-potential point in the desired mode(s) of operation of the second patch antenna 110, it does not significantly disturb the second patch antenna's antenna 110's operation.

Please replace paragraph 0029 (page 10, line 11 through page 11, line 5) with the following amended paragraph:

[0029] The structure described thus far supports two orthogonal linear polarizations in each frequency band (patch element). Additionally, the two beginning RF signals corresponding to their respective linear polarizations can be further manipulated to yield two mathematically orthogonal circular polarization states (right-hand-circularly-polarized and left-hand-circularly-polarized, or RHCP and LHCP) from the same structure. This is done by applying a + or -90 degree phase shift to the two base RF signals, before they are each further split and shifted 180 degrees to form differential feeds. In practice, this is often done using a 90-degree hybrid, so that RHCP (right hand circular polarization) and LHCP (left hand circular polarization) are

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simultaneously available from the antenna system. Hence, each of the patch antennas 105 and 110 can further provide the two circular polarization states, RHCP and LHCP. As an example, one or both patch antennas preferably are dual-polarized. The two linear polarizations' signals for a patch element are combined to give circular polarization. In the embodiment in which each patch antenna has four feed points feedpoints, grouped by twos into two pairs (i.e., two differential feeds--[[()]one differential feed pair per linear polarization), the two differential feed pairs can be further manipulated to produce instead two circular polarization feed signals. It will be appreciated by those of ordinary skill in the art that the entire hierarchy can be repeated for the other patch antenna.

Please replace paragraph 0030 (page 11, lines 6-13) with the following amended paragraph:

[0030] FIG. 5 is an isometric view from the bottom of one embodiment of the stacked patch antenna 100. As illustrated, the ~~one or more~~ ground planes 130 are preferably comprised of a single piece of copper plating to provide a consistent ground reference. The control circuit board 120 is coupled both electrically and mechanically to the ~~one or more~~ ground planes 130 as previously described herein. A battery 500, [[or]] a DC bias voltage applied through the transmission transmissions lines connecting the probe antenna to the instrumentation, or some other fixed power supply provides power to the control circuit board 120 for operation.